

# NARROMINE WEST SOLAR FARM

## Reflective Glare Assessment

### Prepared for:

Providence Asset Group  
704/99 Bathurst Street  
SYDNEY NSW 2000

SLR Ref: 620.30234-R01  
Version No: -v1.0  
February 2021



## PREPARED BY

SLR Consulting Australia Pty Ltd  
ABN 29 001 584 612  
Tenancy 202 Submarine School, Sub Base Platypus, 120 High Street  
North Sydney NSW 2060 Australia

T: +61 2 9427 8100  
E: sydney@slrconsulting.com www.slrconsulting.com

## BASIS OF REPORT

This report has been prepared by SLR Consulting Australia Pty Ltd with all reasonable skill, care and diligence, and taking account of the timescale and resources allocated to it by agreement with Providence Asset Group (the Client). Information reported herein is based on the interpretation of data collected, which has been accepted in good faith as being accurate and valid.

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## DOCUMENT CONTROL

Reference	Date	Prepared	Checked	Authorised
620.30234-R01-v1.0	25 February 2021	Peter Hayman	Dr Peter Georgiou	Dr Neihad Al-Khalidy

## EXECUTIVE SUMMARY

SLR Consulting Australia Pty Ltd (SLR) has been engaged by Providence Asset Group to carry out a Reflective Glare assessment of the proposed Narromine West Solar Farm (the "Project"). The Project is located on Dandaloo Road, just over 1 km west of the outskirts of the township of Narromine and is close to the nearby Narromine Aerodrome, being just under 1 km south of the aerodrome's nearest runway thresholds.

The proposed (up to) 5 MWac facility (refer **Section 2**) will comprise 12,348 solar PV panels within a 15 ha project site area. The 540 W panels, measuring approximately 2.26 m by 1.13 m, will be positioned as currently understood on single-axis trackers oriented north-south with a spacing of 6.25 m.

The following potential glare conditions have been considered:

- Daytime Reflective glare (and glint) arising from the solar PV panels within the facility:
  - . Aviation Sector Reflective Glare;
  - . Motorist "Disability" Reflective Glare and Pedestrian "Discomfort" Reflective Glare;
  - . Rail Operator Reflective Glare;
  - . Industrial critical machinery operators (heavy vehicles, etc) Reflective Glare; and
  - . Residential "Nuisance" Glare.
- Night-time Illumination glare if any 24/7 operational security lighting is incorporated into the Project in the future; none is currently planned.

### Aviation-Related Potential Glare

Quantitative analysis using the FAA-SGHAT software tool has shown that there will be nil glare from the Project at Narromine Aerodrome with the solar array in normal tracking mode, ie panels tilting  $\pm 60^\circ$ .

There is potential for glare if panels need to be left at a near horizontal angle. Leaving the solar array with either an eastwards or westwards fixed tilt angle of at least  $15^\circ$  would eliminate this occurrence. This will also eliminate any potential for glider operational glare on Runway 36.

### Motorist, Rail Traffic and Residential Glare

There will be nil glare from the Project in relation to road traffic, rail traffic and surrounding residential receivers under the standard operational  $\pm 60^\circ$  tilt angle scenario.

There is potential for reflection visibility, although not reflective glare, to nearby residential receivers if solar panels are left in a FIXED TILT horizontal or near horizontal position (eg for maintenance, during construction, under back-tracking mode, etc) - mainly applying to Receiver 4 east of the site. To eliminate the visibility of reflections entirely at Receiver 4, perimeter landscaping along the eastern perimeter of the site or avoiding fixed tilt angle east scenarios during late afternoon of winter months has been recommended.

Night-time lighting is not currently incorporated into the Project. If 24/7 lighting is required in the future for operational purposes, there should be negligible impact, assuming the lighting design is in accordance with AS 4282-1997 *Control of the Obtrusive Effect of Outdoor Lighting*. This would also address any potential adverse eco-lighting issues in relation to nocturnal fauna within and surrounding the site, although, as far as is known, no biodiversity issues have been identified in relation to the Project. Any future lighting design should also be checked against CASA's NASF Guidelines (E & F).

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## EXECUTIVE SUMMARY

When key Project decisions are finalised during detailed design (eg final panel selection, mounting details, etc), the present analysis should be re-visited to confirm the conclusions set out above if key assumptions made in the analysis change significantly.



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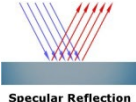

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## Abbreviations and Definitions

### Terms relevant to Daytime Reflective Glare

PV Panel	Photovoltaic (PV) panels are designed to absorb solar energy and retain as much of the solar spectrum as possible in order to produce electricity.
Glare	Glare refers to the reflections of the sun off any reflective surface, experienced as a source of excessive brightness relative to the surrounding diffused lighting. Glare covers reflections: <ul style="list-style-type: none"> <li>Which can be experienced by both stationary and moving observers (the latter referred to as “glint”).</li> <li>Which are either specular or diffuse.</li> </ul>
Specular	A reflection which is essentially mirror-like – there is virtually no loss of intensity or angle dispersion between the incoming solar ray and outgoing reflection. 
Diffuse	A reflection in which the outgoing reflected rays are dispersed over a wide (“diffuse”) range of angle compared to the incoming (parallel) solar rays, typical of “rougher” surfaces. 
KVP	Key View Points (KVPs) are offsite locations where receivers of interest have the potential to experience adverse reflective glare.

### Terms relevant to Night-Time Illumination

Luminous intensity	The concentration of luminous flux emitted in a specific direction. Unit: candela (Cd).
Luminance <b>AS 1158.2:2005</b>	This is the physical quantity corresponding to the brightness of a surface (e.g. a lamp, luminaire or reflecting material such as façade glazing) when viewed from a specified direction. Unit: Cd/m <sup>2</sup>
Illuminance <b>AS 1158.2:2005</b>	This is the physical measure of illumination. It is the luminous flux arriving at a surface divided by the area of the illuminated surface – the unit is lux (lx) ... 1 lx = 1 lm/m <sup>2</sup>  The term covers both “Horizontal Illuminance” (the value of illuminance on a designated horizontal plane at ground level) and “Vertical Illuminance” (the value of illuminance on a designated vertical plane at a height of 1.5m above ground level).
Glare <b>AS 1158.2:2005</b>	Condition of vision in which there is a discomfort or a reduction in the ability to see, or both, caused by an unsuitable distribution or range of luminance, or to extreme contrast in the field of vision. Glare can include: <ul style="list-style-type: none"> <li>(a) Disability Glare – glare that impairs the visibility of objects without necessarily causing discomfort.</li> <li>(b) Discomfort Glare – glare that causes discomfort without necessarily impairing the visibility of objects.</li> </ul>
Threshold Increment (TI) <b>AS 4282:2019</b>	TI is the measure of disability glare expressed as the percentage increase in contrast required between an object and its background for it to be seen equally well with a source of glare present. Higher TI values correspond to greater disability glare.

# 1 INTRODUCTION

SLR Consulting Australia Pty Ltd (SLR) has been engaged by Providence Asset Group to carry out a Reflective Glare assessment of the proposed Narromine West Solar Farm (the “Project”). The Project is located on Dandaloo Road, just over 1 km west of the outskirts of the township of Narromine and is close to the nearby Narromine Aerodrome, being just under 1 km south of the nearest runway threshold of Narromine Aerodrome’s Runway 04/22.

The following potential glare conditions have been considered:

- Daytime Reflective glare (and glint) arising from the solar PV panels within the facility
- Night-time Illumination glare from 24/7 operational security lighting within the facility

## 1.1 Structure of Report

The remainder of this report is structured as follows:

- **Section 2** describes the Project and surrounding environment.
- **Section 3** describes the range of receptors surrounding the site with the potential to experience adverse reflective glare (or glint).
- **Section 4** presents the acceptability criteria used for the study.
- **Section 5** addresses the assumptions made in the glare impact analysis.
- **Section 6** presents the results of the glare impact analysis of the Project.
- **Section 7** presents the conclusions of the study.



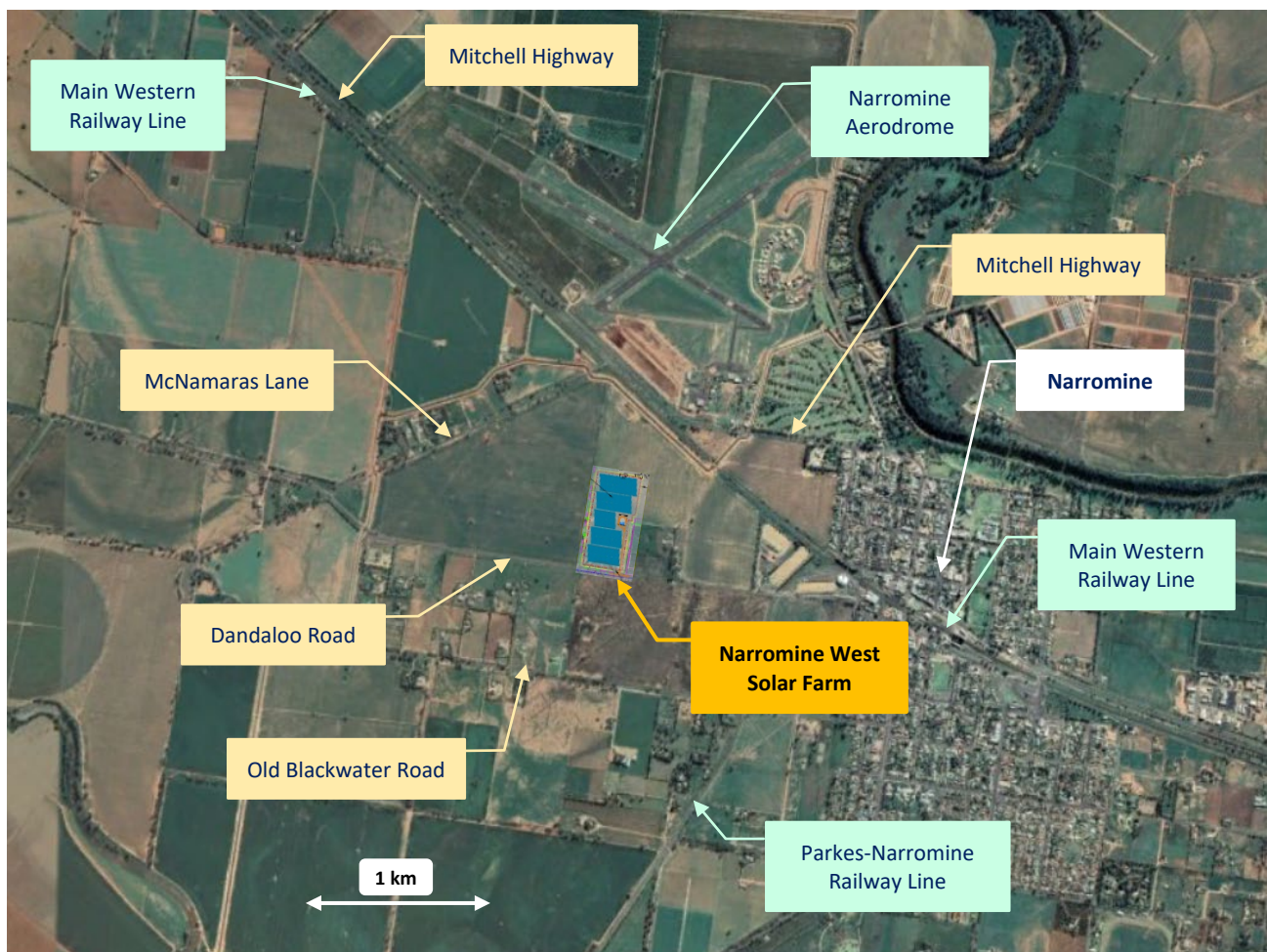
## 2 PROPOSED NARROMINE WEST SOLAR FARM PROJECT

### 2.1 Site Location

The Project is seeking approval for an (up to) 5 MWac photovoltaic (PV) solar plant occupying a 15 ha area as shown in **Figure 1**. The Project is located on Dandaloo Road, just over 1 km west of the outskirts of the township of Narromine and is close to Narromine Aerodrome, being just under 1 km south of the nearest runway threshold of Narromine Aerodrome's Runway 04/22.

The land required for the Project has been subject to constraints identified by site investigation, i.e. native vegetation, and areas of cultural or heritage significance. The plan of the Project has been developed following completion of these site investigations and the assessment of any constraints and their impact.

**Figure 1** Narromine West Solar Farm - Location Map



## 2.2 Site Description and Key Project Components

From a Reflective Glare point of view, the key components of the Project are:

- the photovoltaic (PV) modules in relation to their daytime reflective glare potential; and
- the facility's security/emergency lighting design in relation to potential night-time illumination glare issues, if such 24/7 lighting is incorporated into the Project – note: none is currently planned.

### Solar Panel Mounted Array – refer Figure 2

The proposed ground-mounted array (refer **Figure 2(a)**) would consist of 147 trackers oriented in a north-south direction, each supporting 84 x 540W solar panels (12,348 panels in total);

- The trackers are “single-axis” capable of rotating solar panels to a maximum of  $\pm 60^\circ$  - refer **Figure 2(b)**;
- The trackers are oriented north-south and spaced 6.25 m apart;
- Individual panels (2.26 m x 1.13 m) reach a maximum height above ground of 2.58 m at their full  $60^\circ$  tilt angle; and
- The northern perimeter of the Project lies just under 1 km south of the two southern thresholds of Narromine Airfield's Runway 04 and Runway 29.

**Figure 2 Narromine West Solar Farm Site Layout**

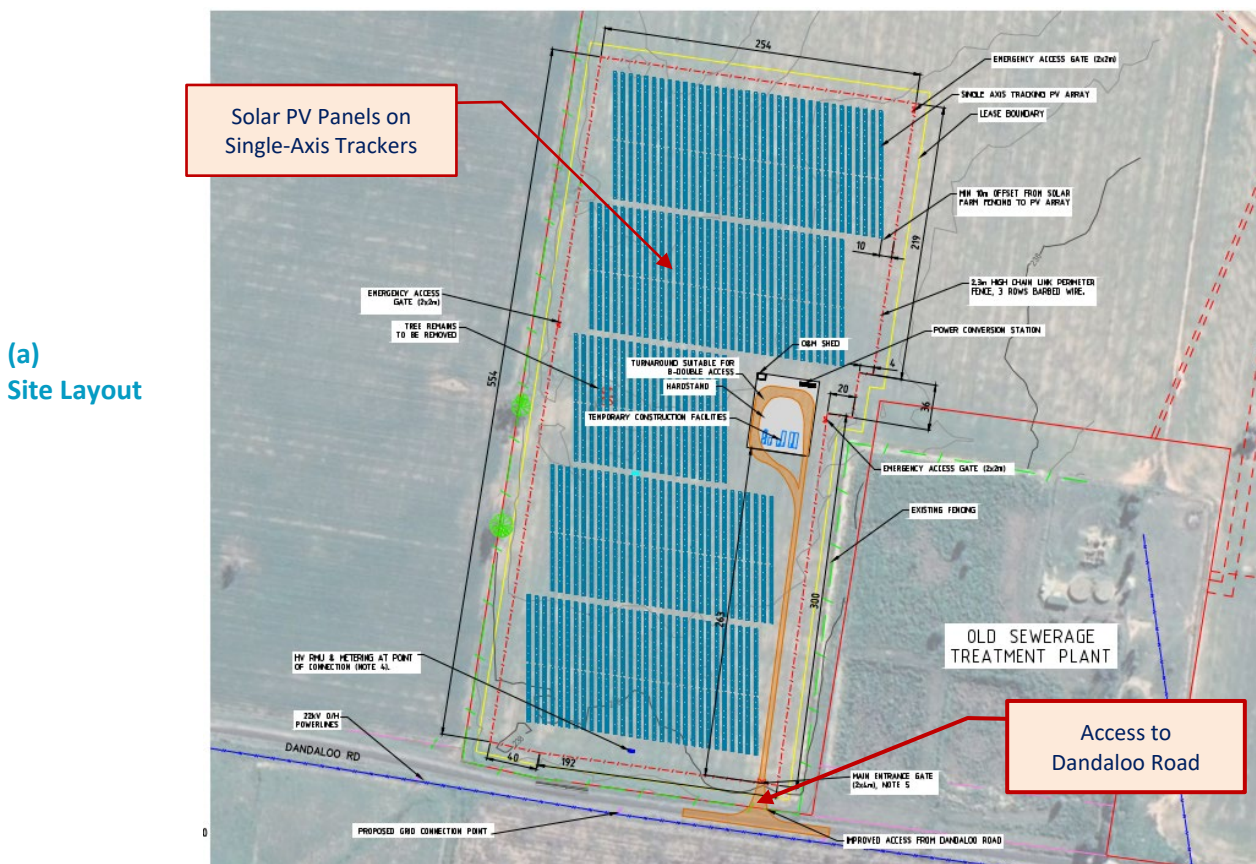
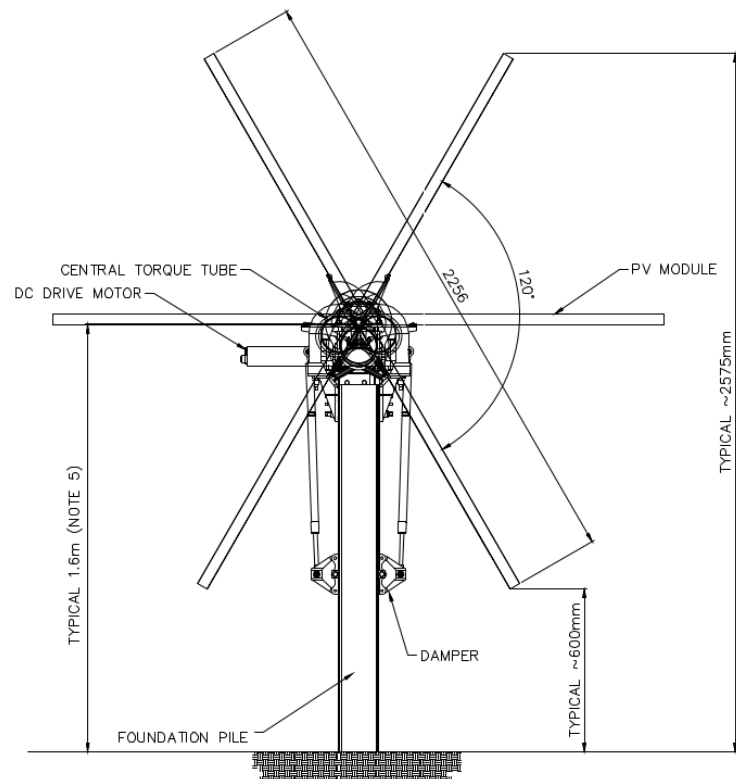


Fig.2 (cont'd)

(b)  
Single-Axis  
Tracker Profile  
(  $\pm 60^\circ$  Tilt )



## 3 RECEIVERS AND ASSOCIATED IMPACTS

### 3.1 Receiver Impacts

The issues of concern in relation to daytime reflective glare and night-time illumination glare and the associated receivers of interest are detailed below.

#### Aviation-Related Glint & Glare (Aircraft, Helicopters, Airport Control Towers)

There have been several documented cases globally, none in Australia, of solar panel installations at airports interfering with Airport Control Tower operations. There is the added potential for reflective glare to impact pilots especially during the latter approach stages of landing, when the line of sight of the pilot is directed downwards.

#### Motorist Traffic Disability Glare on the surrounding road network

The issue of concern here is the potential occurrence of Traffic Disability Glare, which most often arises from incoming solar rays striking a reflective surface at a moderately high (“glancing”) incident angle (typically greater than 70°) and altitude angle less than 25° (altitude angles greater than this would be intersected and obstructed by a typical windscreen roof-line).

#### Train Driver Disability Glare on the surrounding rail network

The issue of concern here is the potential impact of reflective glare interfering with or distracting a train operator’s activities or the potential for reflections to obscure railway signals.

#### Industrial Critical Machinery Operators (draglines, heavy trucks, etc)

The issue of concern here is the potential impact of reflective glare interfering with or distracting the operators of critical industrial machinery.

#### Residential Nuisance Glare on surrounding receivers

The issue of concern here is the potential “nuisance” caused by extended periods of reflective glare.

Nearest neighbours may also be impacted by light spill from night-time illumination, although it is noted that none is currently planned for the Project.

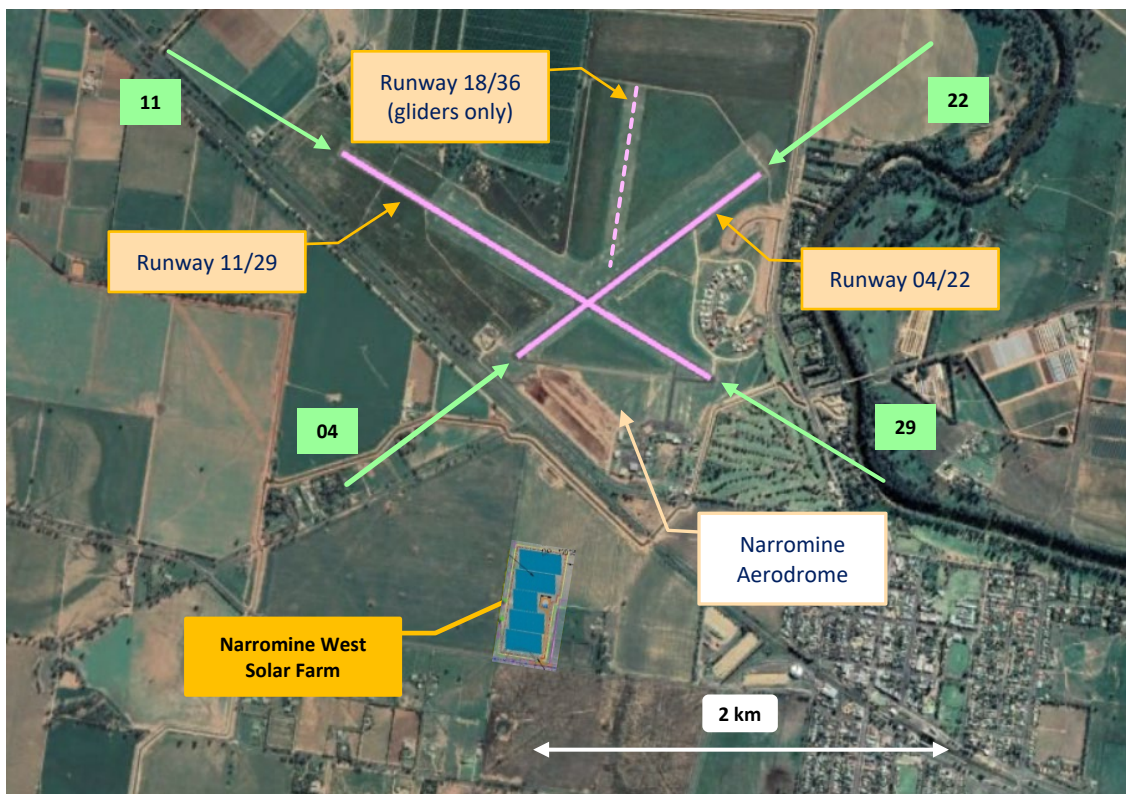
### 3.2 Nearest Receiver Locations

Receivers of interest relevant to the Project are shown in:

- Figure 3**      Nearest aerodrome;
- Figure 4**      Surrounding road network;
- Figure 5**      Surrounding rail network; and
- Figure 6**      Nearest representative residential receivers.



**Figure 3 Nearest Aerodrome to Project Site**

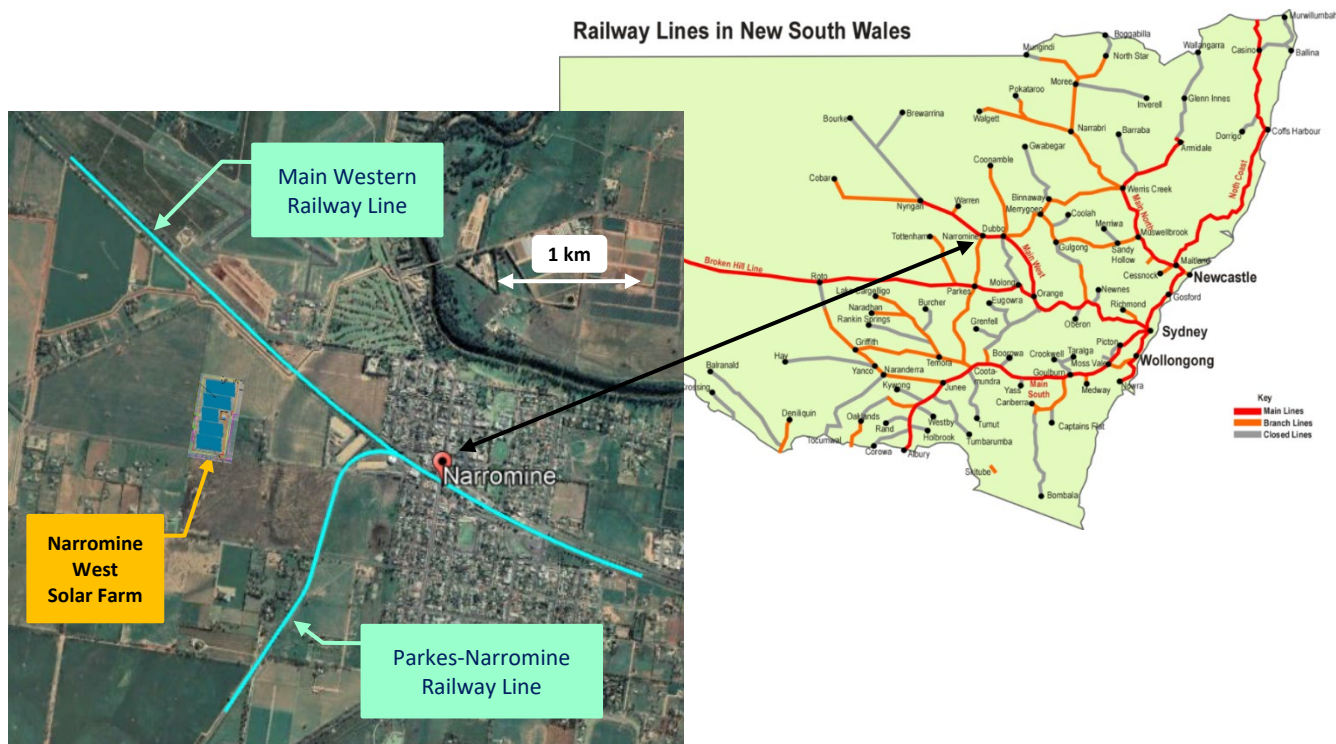


**Figure 4 Surrounding Road Network**





**Figure 5 Surrounding Rail Network and NSW Rail Map**



**Figure 6 Nearest Representative Residential Receivers**



## 4 GLARE ACCEPTABILITY CRITERIA

In relation to **daytime** reflective glare impact, the Project contains the following elements of interest:

- PV modules using solar panels on the Project ground array.

In relation to **night-time** illumination glare impact, the Project may, in the future, include the following elements of interest:

- 24/7 lighting for access roads to enable site maintenance, fire and other emergency events, and 24/7 lighting for the on-site Operations & Maintenance building and power conversion unit which provide connection to the local distribution network.

Night-time illumination is not presently incorporated in the current Project design.

### 4.1 Aviation Sector Reflective Glare

The impact of solar PV systems on aviation activity is something that solar developers today are addressing more and more often, given the (global) proliferation of solar projects, in particular those located either within or around airport precincts.

#### US FAA

In relation to the potential impact of solar PV systems on aviation activity, guidance is available from the US FAA which regulates and oversees all aspects of American civil aviation. On the basis of the above and other technical R&D references, the FAA issued a Technical Guidance Policy in 2010 and a subsequent (and over-riding) Interim Policy in 2013. The Technical Guidance Policy was updated in 2018.

- FAA, *“Technical Guidance for Evaluating Selected Solar Technologies on Airports”*, Federal Aviation Administration, Washington, D.C., November 2010.
- FAA, *“Interim Policy, FAA Review of Solar Energy System Projects on Federally Obligated Airports”*, Federal Register, Oct. 23, 2013.
- FAA, *“Technical Guidance for Evaluating Selected Solar Technologies on Airports”*, Federal Aviation Administration, Washington, D.C., Version 1.1, April 2018.

In support of the above, the FAA contracted Sandia Labs to develop their **Solar Glare Hazard Analysis Tool** (SGHAT) software as the standard tool for measuring the potential ocular impact of any proposed solar facility on a federally obligated airport. SGHAT utilises the Solar Glare Ocular Hazard Plot to determine and assess the potential for glare.

SGHAT is described in the following references:

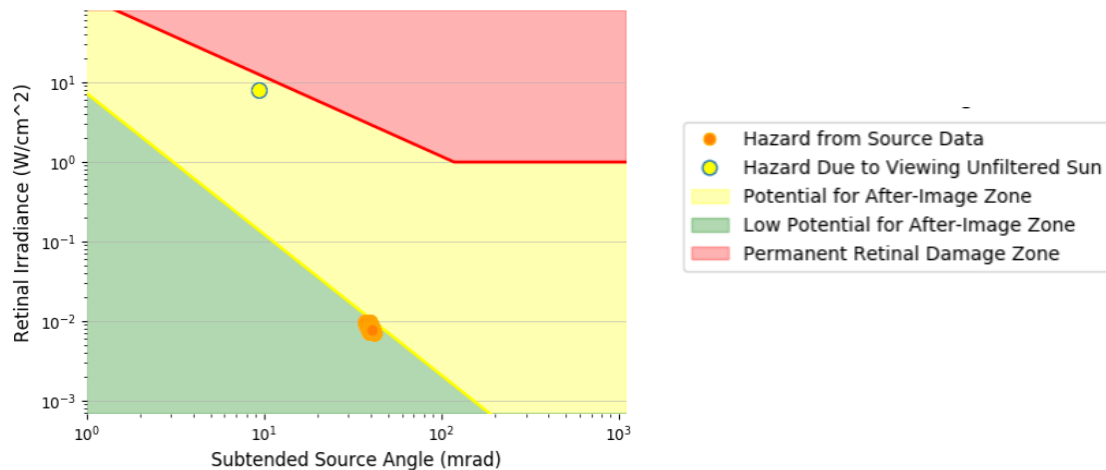
- Ho, C.K., Ghanbari, C.M. and Diver, R.B., *“Methodology to Assess Potential Glint and Glare Hazards from Concentrating Solar Power Plants: Analytical Models and Experimental Validation”*, J. Solar Engineering, August 2011, Vol.133, 031021-1 to 031021-9.
- Ho, C.K. & Sims, C., *“Solar Glare Hazard Analysis Tool (SGHAT) User’s Manual v2.0”*, Sandia National Laboratories, Albuquerque, NM. August 2013.

A sample Solar Glare Ocular Hazard Plot is shown in **Figure 7**. The analysis contained in this plot is derived from solar simulations that extend over the ENTIRE CALENDAR YEAR in 1-MINUTE intervals, sunrise to sunset.

The SGHAT criteria state that a proposed solar facility should satisfy the following:

- Airport Traffic Control Tower (ATCT) cab: NO Glare
- Final approach paths for landing aircraft: Glare to NOT exceed “Low Potential for After-Image”

**Figure 7 Example Solar Glare Ocular Hazard Plot (SGHAT Software Output)**



In **Figure 7**, the following is noted:

- SGHAT ocular impact is a function of both the “retinal irradiance” (ie the light seen by the eye) and “subtended source angle” (ie how wide an arc of view the light appears to be arriving from).
- SGHAT ocular impact falls into three categories:
  - . GREEN: low potential to cause “after-image”
  - . YELLOW: potential to cause temporary “after-image”
  - . RED: potential to cause retinal burn (permanent eye damage)
- “After Image” is the term applied to a common retinal phenomenon that most people have experienced at some point or other, such as the effect that occurs when a photo with flash is taken in front of a person who then sees spots in front of their eyes for a few seconds. A more extreme example of “after-image” occurs when staring at the sun. “After-image” (also known as “photo bleaching”) occurs because of the de-activation of the cells at the back of the eye’s retina when subjected to a very bright light.
- The SGHAT plot provides an indication of the relative intensity of both the incoming reflection and the sources of light itself (ie the sun).
  - . The occurrence of glare is shown in the plot as a series of **orange circles**, one circle for each minute that a reflection is visible.
  - . A reference point is also shown in each SGHAT plot, the **green circle**, representing the hazard level of viewing the sun without filtering, ie staring at the sun.
- In **Figure 7**, it can be seen that the reflection visible by the receiver is roughly 1,000 times less intense than the light from the sun.



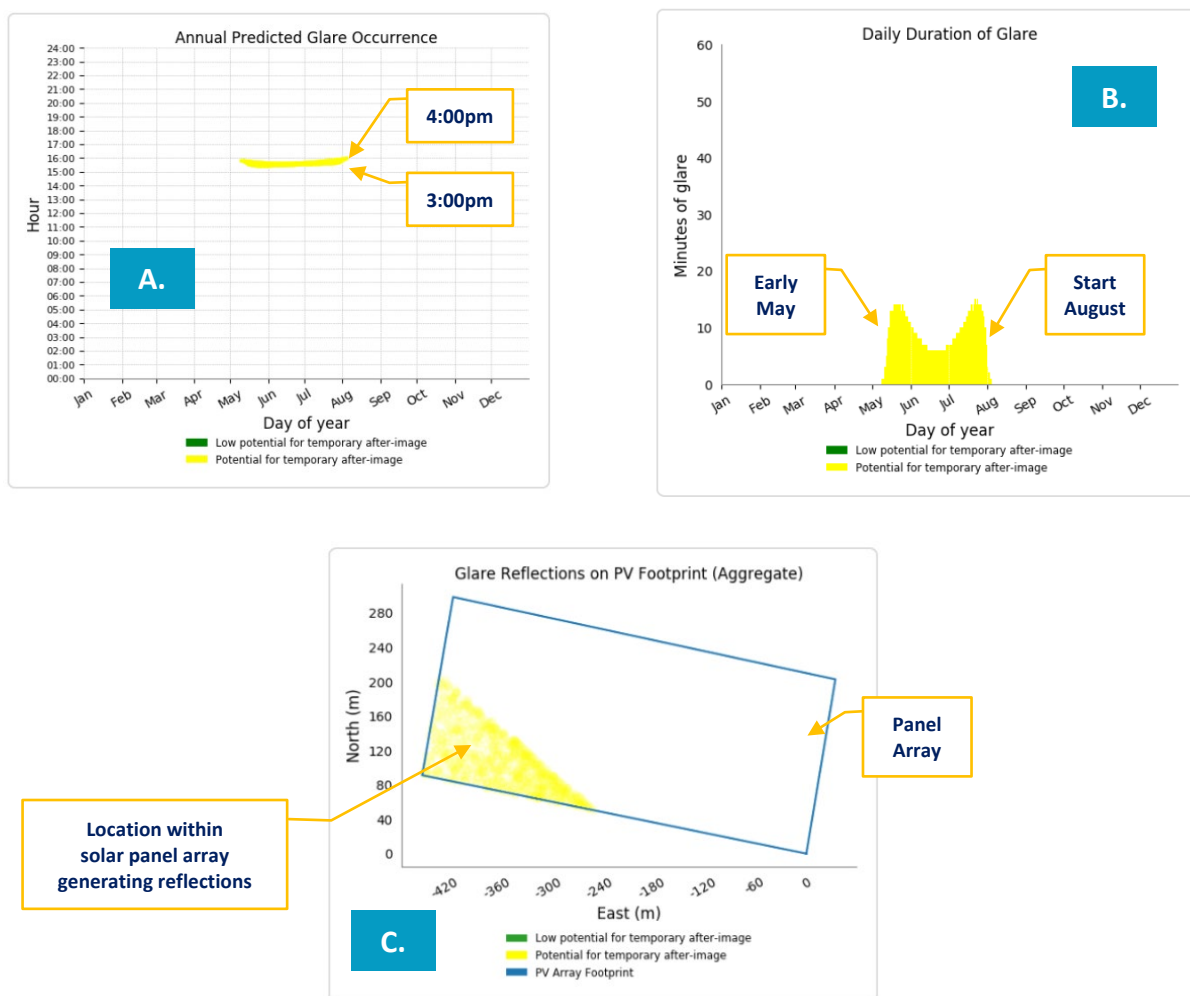
- Finally, in relation to PV Solar facilities, it is important to note that the third SGHAT Ocular Plot “RED” category is **not possible**, since PV modules DO NOT FOCUS reflected sunlight.

### Additional Information Available with the SGHAT Analysis Tool

In addition to the above “assessment” output, the SGHAT software package also produces information which reveals the extent of visibility of reflections at any chosen receiver position, regardless of whether the reflections constitute a glare condition or not – an example is shown in **Figure 8**.

- Figure 8-A:** shows the am/pm time periods when reflections occur at a specific position throughout the year, in this case typically between around 3:30pm and 4:00pm.
- Figure 8-B:** shows the months during the year and the minutes per day when reflections occur at a specific position, in this case from early-May to the start of August.
- As noted above, this information is made possible because the SGHAT analysis covers the entire solar annual cycle in 1-minute intervals to ascertain any potential impacts on surrounding receivers.
- Finally, **Figure 8-C** shows WHERE within the solar farm panel array the reflection rays of interest are emanating from, in this case from panels near the southwest corner.

**Figure 8 Example Solar Glare Output Plots (SGHAT Software Output)**



## SGHAT Analysis Covering Glider Operations

Narromine Airport has three runways available for use by gliders:

- Two of the glider runways coincide with the asphalt/grass runways used by commercial and general aviation: Runway 11/29 and Runway 04/22;
- Runway 18/36 is solely for the use of gliders.

When carrying out SGHAT calculations for commercial and general aviation, a common assumption is made regarding flight angle on landing, namely a glide path of 3°. Actual operations of such aircraft seldom vary from this angle.

Gliders on the other hand have significant flexibility in relation to landing flight path glide angle, in particular, gliders can accommodate considerably higher glide angles on their approach path to landing.

SGHAT however can only accommodate a standard 3° glide path on landing. Consequently, when carrying out SGHAT analyses for airfields having glider operations, SGHAT analysis has to be viewed with the potential to varying outcomes if steeper glide paths are assumed.

## 4.2 Motorist “Disability” Glare and Pedestrian “Discomfort” Glare

The criteria commonly used by Australian Local Government Authorities to assess the acceptability or otherwise of potential adverse reflections from glazed façade systems onto surrounding roadways and pedestrian crossings utilise the so-called **Threshold Increment (TI)** Value of the reflection condition.

### TI Value Definition

AS/NZS 4282:2019 defines Threshold Increment (TI) as:

*"the measure of disability glare expressed as the percentage increase in contrast required between an object and its background for it to be seen equally well with a source of glare present. Note: Higher values of TI correspond to greater disability glare."*

The TI Value is calculated as the ratio of “veiling” luminance (eg from a reflection) to the overall average background (“adaptation”) luminance, with the necessary constant and exponent parameters provided in AS 1158.2:2005.

The formula for calculating the TI Value is ...  $TI = 65 L_v / L_{tb}^{0.8}$ , where:

- $L_v$  = veiling luminance from a source of interest ( eg reflection ) – Cd/m<sup>2</sup>
- $L_{tb}$  = so-called “adaptation” luminance ( total background ) – Cd/m<sup>2</sup>

### TI Value Acceptability Criteria

The acceptability criteria adopted by Australian Local Government Authorities to assess the acceptability or otherwise of potential adverse reflections from glazed façade systems onto surrounding roadways and pedestrian crossings utilise the so-called **Threshold Increment (TI)** Value of the reflection condition (refer above for definition and calculation equations).

For (Motorist) Traffic Disability Glare, the TI Value should remain:

- Below 10 for major roads
- Below 20 for minor roads

For Pedestrian Discomfort Glare, the TI Value should remain:

- Below 2 at critical locations such as pedestrian crossings
- Below 3 for other locations

For the present study, Pedestrian Discomfort Glare is relevant to the potential for residential nuisance glare from surrounding receivers.

It should be noted that while Pedestrian Discomfort Glare can occur over a wide range of solar altitude angles, in most such instances, a pedestrian has the ability to adjust their line of sight to a more horizontal view away from the glare source, thereby rendering TI values essentially negligible.

### 4.3 Rail Operators Reflective Glare

Almost all Australian Rail Authorities have guidelines covering glare in general (ie not specific to solar PV panel glare) aimed at avoiding discomfort/distraction to train operators and obscuring train signals. Most guidelines refer either to Table 2.10 of AS 1158.3.1 for the TI Value criterion and/or Table 3.2 of AS 1158.4 for the Cd (Candela) criterion associated with the control of glare.

- For Rail Traffic Disability Glare, the relevant AS1158 criteria are:
  - The TI Value should remain below 20%
  - The Cd Value at 70° incidence should remain below 6,000.

### 4.4 Residential “Nuisance” Glare

Instances of documented nuisance glare associated with solar PV panels (grid-scale, industrial or residential) and nearby residential receivers have been relatively infrequent globally, especially given the widespread and rapid increase in the take-up of residential solar panels in Australia and elsewhere.

There are currently no national or state guidelines in Australia governing the acceptability or otherwise of residential nuisance glare specific to solar PV.

Existing guidance that exists in relation to solar panels from state governments typically covers installation audits and compliance checks. Additional guidance in relation to compliance with Australia Standards is provided by:

**Clean Energy Council**

Website: <https://www.cleanenergycouncil.org.au/industry/products/modules>

Accordingly, to assist in addressing residential nuisance glare, reference has been made of the concepts used for glare acceptability criteria outlined in the preceding sections.

## 4.5 Industrial Critical Machinery Operations

There are currently no (Australian) national or state guidelines governing the acceptability or otherwise of reflective glare for industrial site critical operations. Instead, the concepts used for acceptability criteria in the preceding sections, in particular Traffic Disability Glare, can assist when dealing with this issue.

The issue most commonly arises in relation to mining operations where machinery operators can be located in elevated locations, eg dragline operations, where a line of sight may be possible to a solar facility located in close proximity. Ports with their observation towers are another potential source of elevated receivers of interest if located adjacent to a solar facility.

No such industrial operations exist in the present case.

## 4.6 Night-Time Illumination Glare

The effect of light spill from outdoor lighting impacting on residents, transport users, transport signalling systems and astronomical observations is governed by AS 4282-2019.

The adverse effects of light spill from outdoor lighting are influenced by a number of factors:

- The topology of the area. Light spill is more likely to be perceived as obtrusive if the lighting installation is located higher up than the observer. Lighting installations are usually directed towards the ground and an observer could hence have a direct view of the luminaire.
- The surrounding area. Hills, trees, buildings, fences and general vegetation have a positive effect by shielding the observer from the light installation.
- Pre-existing lighting in the area. Light from a particular light source is seen as less obtrusive if it is located in an area where the lighting levels are already high, eg in cities. The same lighting installation would be seen as far more bothersome in a less well-lit residential area.
- The zoning of the area. A residential area is seen as more sensitive compared to commercial areas where high lighting levels are seen as more acceptable.

Typical illuminance levels for a variety of circumstances are given in **Table 1** for comparison.

**Table 1 Typical Illuminance Levels for Various Scenarios**

Lighting Scenario	Horizontal Illuminance (lux)
Moonless overcast night	0.0001
Quarter Moon	0.01
Full Moon	0.1
Twilight	10
Indoor office	300
Overcast day	1,000
Indirect sunlight clear day	10,000-20,000
Direct sunlight	100,000-130,000

Recommended criteria of light technical parameters for the control of obtrusive lighting are given in **Table 2**. The vertical illuminance limits for *curfew hours* apply in the plane of the windows of habitable rooms or dwellings on nearby residential properties. The vertical illuminance criteria for *pre-curfew hours* apply at the boundary of nearby residential properties in a vertical plane parallel to the boundary.

Values given are for the direct component of illuminance, i.e. no reflected light is taken into account.

- Limits for luminous intensity for *curfew hours* apply in directions where views of bright surfaces of luminaires are likely to be troublesome to residents, from positions where such views are likely to be maintained.
- Limits for luminous intensity for *pre-curfew hours* apply to each luminaire in the principal plane, for all angles at and above the control direction.

**Table 2 Recommended Maximum Values of Light Technical Parameters (AS4282-1997)**

Light Technical Parameter	Time of Operation	Commercial Areas	Residential Areas	
			Light Surrounds	Dark Surrounds
Illuminance in vertical plane ( $E_v$ )	Pre-curfew hours	25 lx	10 lx	<b>10 lx</b>
	Curfew hours	4 lx	2 lx	<b>1 lx</b>
Luminous Intensity emitted by luminaires (I)	Pre-curfew hours	7,500 Cd (for a medium to large area with Level 1 control)	100,000 Cd (for a large area with Level 1 control)	100,000 Cd (for a large area with Level 1 control)
	Curfew hours	2,500 Cd	1,000 Cd	500 Cd

The Project is located outside the Narromine township area and has the potential to impact on surrounding residential properties – refer **Figure 6**. As these properties are not located within township environs proper, they would therefore be classed as being in a residential area with “Dark Surrounds” - refer **Table 2**.

The applicable limits for adverse spill light will depend on the time of operation for the lighting installation.

For the Project, it is possible that internal access roads and any equipment buildings in particular, will be operational 24/7, suggesting the application of the more restrictive limit relevant to *curfew hours*.

Accordingly:

- Light spill from the Project onto the facades of the surrounding residential dwellings should be kept below 1 lux during curfew hours

It is noted that night-time lighting is not currently incorporated into the Project.

Finally, it has been known for some time that night-time artificial lighting has the potential to disrupt the natural behaviour of nocturnal fauna species such as arboreal mammals, large forest owls and microbats. The standards mentioned above do not contain limiting lux levels in relation to the mitigation of such eco-lighting impacts.

Mitigation recommendations in relation to adverse eco-lighting therefore centre on feasible night-time lighting minimisation, bearing in mind the provision of appropriate health and safety and security conditions given the nature of the site. Biodiversity associated with the Project is discussed in the Flora and Fauna Assessment Report prepared for the Project. As far as is known, no adverse eco-lighting issues are apparent.

## 5 GLARE IMPACT ASSESSMENT - ASSUMPTIONS

The following potential glare conditions have been considered:

- Daytime Reflective glare (and glint) arising from the solar PV panels
- Night-time Illumination glare if any 24/7 operational security lighting is located within the site

### 5.1 Assumptions – Solar Panel Geometry

The glare assessment discussed in detail in following sections is based on the following assumptions:

- The solar panel array trackers are “single-axis” capable of rotating solar panels to a maximum of  $\pm 60^\circ$ .
- The trackers are oriented north-south and spaced 6.25 m apart.
- Individual panels (2.26 m x 1.13 m) reach a maximum height above ground of 2.58 m at their full  $60^\circ$  tilt angle.
- The southern perimeter of the Project runs along Dandaloo Road. The northern perimeter of the site lies just under 1 km from the nearest threshold of Narromine Aerodrome’s Runway 04/22. The northeast corner of the site lies approximately 350 m from the nearest point of the Main Western Railway Line. The south corner of the site lies approximately 800 m from the nearest point of the Parkes-Narromine Railway Line.

### 5.2 Project Site Solar Angles – Annual Variations

One of the challenging issues encountered with daytime solar panel glare is the varying nature of the reflections, whose duration will vary with time of day and day of the year as the sun’s rays follow variable incoming angles between the two extremes of:

- summer solstice - sunrise incoming rays from just south of east, maximum angle altitude rays at midday, sunset incoming rays from just south of west
- winter solstice - sunrise incoming rays from the northeast, minimum angle altitude rays at midday, sunset incoming rays from the northwest

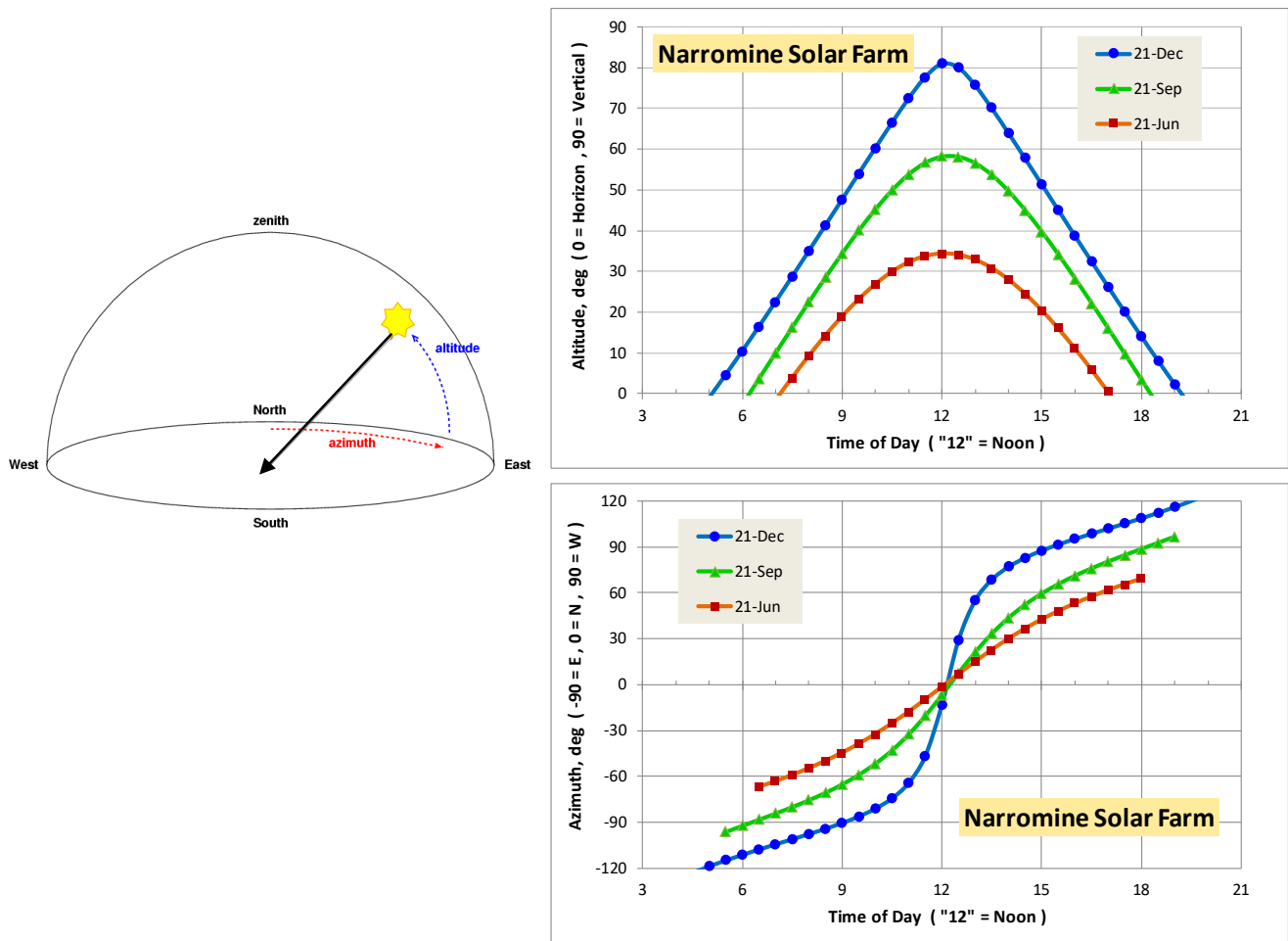
Any solar glare analysis must take into account the complete cycle of annual reflection variations noted above.

The potential range of incoming solar angles at the Project site relevant to daytime glare is shown in **Figure 9** with relevant critical angles summarised in **Table 3**.

**Table 3 Key Annual Solar Angle Characteristics for Project Site**

Day of Year	Sunrise	Sunset	Azimuth Range (sunrise-sunset)	Max Altitude
Summer Solstice	5:06 am	7:13 pm	118.1° E of North to 118.1° W of North	80.9°
Equinox	6:13 am	6:15 pm	90.7° E of North to 90.7° W of North	58.2°
Winter Solstice	7:09 am	5:02 pm	62.0° E of North to 62.0° W of North	34.3°

**Figure 9 Project Site Incoming Solar Angle Variations**



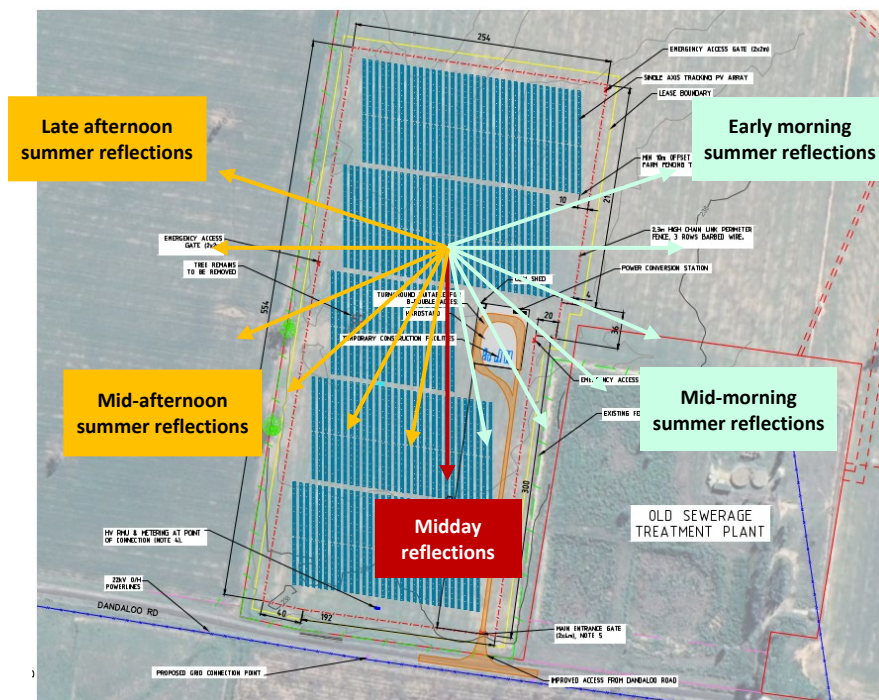
### 5.3 Project Solar Reflections

The project will use single-axis tracking panels (with the axis of rotation oriented north-south) as described in **Section 2.2**. In “plan” view, reflections from the Project’s panels will be directed as shown in **Figure 10** for a representative area of panels, with the direction of reflected rays shown for typical mid-summer days.

As a result of the tracking motion of the solar panels throughout the day, reflections will generally be directed upwards and hence not visible by ground-based receivers at roughly the same elevation as the facility. Where such reflections can be observed by surrounding elevated receivers they would typically be seen as “low incidence” reflections with corresponding low reflectivity. This is the inevitable outcome of the objective of maximising the solar gain of each panel (where the reflectivity would ideally be minimal) and justifying the additional cost of using a tracking system for the panels which follows the sun, rather than a fixed panel system.



**Figure 10 Potential Solar PV Panel Reflection Angles from the Project (typical mid-summer)**



## 5.4 Solar Panel Reflectivity

Solar PV panels are designed to capture (absorb) the maximum possible amount of light within the layers below the front (external) surface. Consequently, solar PV panels are designed to minimise reflections off the surface of each panel. Reflections are a function of:

- the angle at which the light is incident onto the panel (which will vary depending on the specific location, time of day and day of the year), and
- the index of refraction of the front surface of the panel and associated degree of diffuse (non-directional) versus specular (directional or mirror-like) reflection which is a function of surface texture of the front module (reflecting) surface.

Some typical reflectivity values (given in terms of the “n” refractive index value) are:

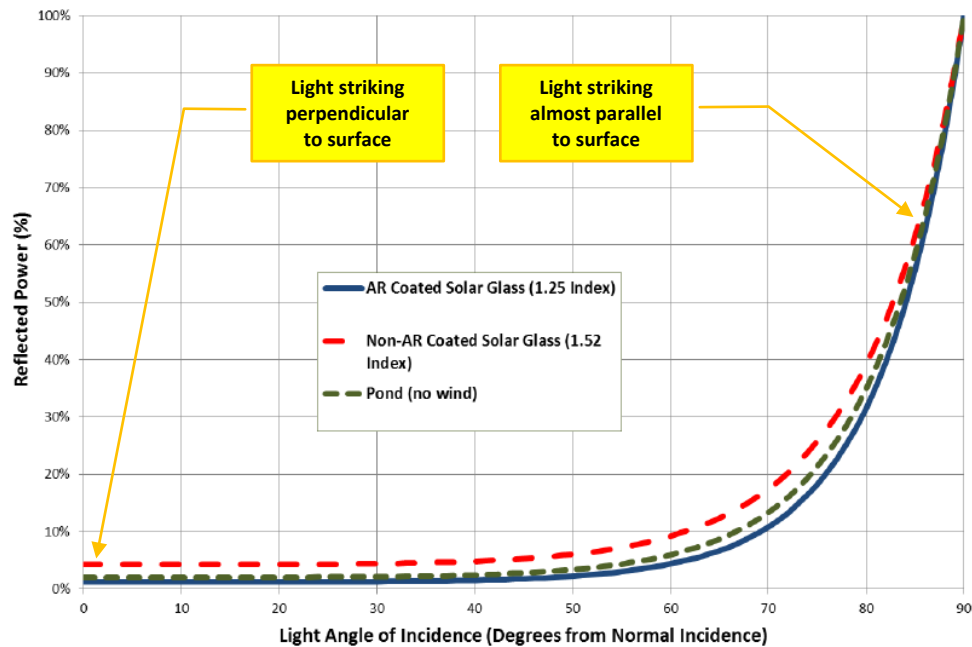
- |                               |          |
|-------------------------------|----------|
| • Snow (fresh, flaky)         | n = 1.98 |
| • Standard Window Glass       | n = 1.52 |
| • Plexiglass, Perspex         | n = 1.50 |
| • Solar Glass                 | n = 1.33 |
| • Solar Glass with AR Coating | n = 1.25 |

Standard PV Solar Panels



Representative reflectivity curves are shown in **Figure 11**.

**Figure 11 Typical Reflectivity Curves as a Function of Incidence Angle**



**Figure 11** shows that:

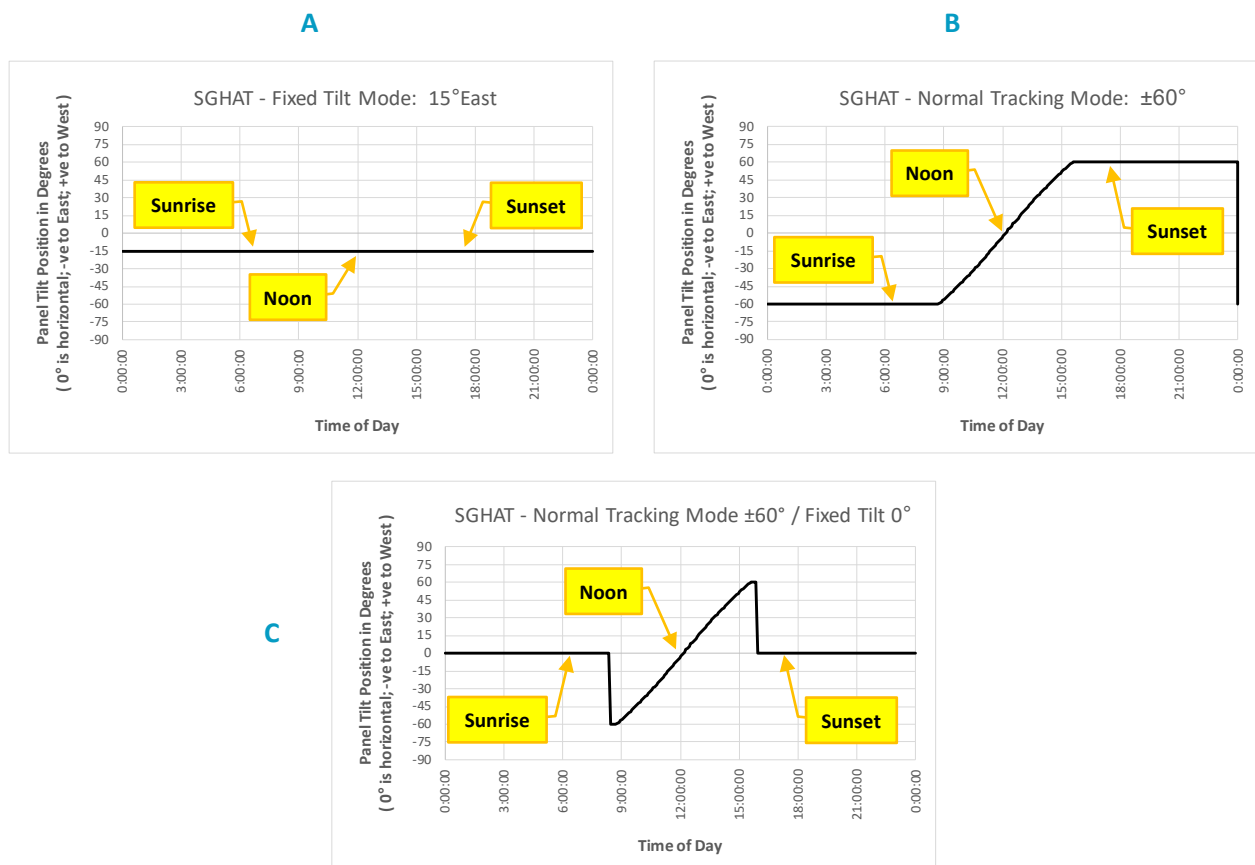
- When an oncoming solar ray strikes the surface of a solar PV panel close to perpendicular to the panel surface (i.e. low “incident” angle), the reflectivity percentage is minimal (less than 5% for all solar panel surface types).
- It is only when an incoming solar ray strikes the panel at a large “incidence” angle, i.e. almost parallel to the panel, that reflectivity values increase. When this happens, reflections become noticeable and potentially at “glare” level for all solar panel surface types.
- However, for very high incidence angle, it would almost always be the case that the observer (motorist, train driver, pedestrian, etc) would perceive reflections coming from virtually the same direction as the incoming solar rays themselves. Such a condition would not constitute a glare situation as the intensity of the incoming solar ray itself would dominate the field of vision perceived by the observer.

## 5.5 Modelling Real-World Tracking Axis Operational Modes

The SGHAT software tool is capable of modelling solar farm panel positions in one of three modes – as shown in **Figure 12**.

- **Fixed Tilt Mode:** in this mode, all panels are assumed to remain at a user-defined fixed angle all day long, eg horizontal, 15°East, 10°West, etc – refer **Figure 12-A**.
- **Normal Tracking Mode:** in this mode, panels move between maximum tilt angles once the sun is above the relevant altitude angle (eg an altitude angle of 30° for  $\pm 60^\circ$  single-axis trackers). They remain at the maximum tilt angles at all other times, switching over during the night – refer **Figure 12-B**.
- **Normal Tracking Mode / Fixed Tilt Stowed:** in this mode, panels move during the day in “normal tracking”: mode, but can then move (instantaneously) to any user-defined fixed tilt angle at all other times – refer **Figure 12-C** where the panels move to a horizontal position (ie 0°) outside of “normal tracking” hours.

**Figure 12 SGHAT Panel Mode Simulation Options**



## “Backtracking” Mode

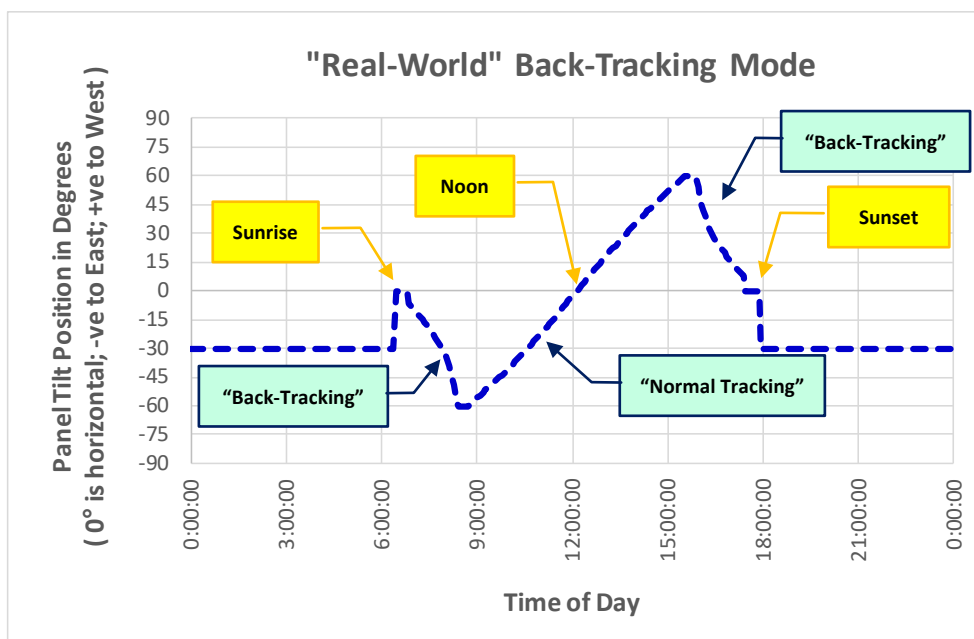
Most recently, sophisticated “back-tracking” operational modes have been developed, typically by the manufacturers of the tracking systems that support solar panels.

- Algorithms are developed (usually fine-tuned during the commissioning stage of a solar facility) aimed at minimising inter-row shading in the early morning and late afternoon. These algorithms are based on the location of a solar facility (ie its latitude), topography, panel row spacing, etc.
- They typically involve constantly re-positioning panels in the early morning and late afternoon starting and ending in a more horizontal position, that “just” avoids inter-row shading.
- During these early morning and late afternoon periods, panel motion is referred to as being in “back-tracking” mode.
- During the remaining hours in the middle of the day, solar panels follow the simplified “normal tracking” mode, ie moving between their maximum ( $\pm 60^\circ$ ) tilt positions.
- There is typically a transition period between the two tracking modes (say ~15 minutes), calculated according to the local site tracking system algorithms.

A real-world example of a “back-tracking” mode is shown in **Figure 13**.

- The sun reaches an altitude angle of  $30^\circ$  in the morning at around 8:30am and again in the afternoon at around 3:45pm. During these hours (ie between around 8:30am and 3:45pm), the panels operate in “normal tracking” mode, ie from  $-60^\circ$  facing East to  $+60^\circ$  facing West.
- From sunrise till 8:30am and from 3:45pm to sunset, the panels operate in “back-tracking” mode, starting at sunrise and ending at sunset in a horizontal position.
- Overnight, the panels are “stowed” in a fixed (in this case,  $-30^\circ$ ) position to minimise wind loading and ensure any moisture (dew or rain) does not pool on the panel overnight and cause increased soiling.

**Figure 13 Example 24-Hour “Back-Tracking” Operational Mode (around equinox)**



SGHAT has not evolved yet to deal with sophisticated “back-tracking” operational modes of the type shown in **Figure 13**. They can only simulate solar farm panel positions in the three simplified modes shown in **Figure 12**.

It will be appreciated therefore that care must be taken when comparing the glare predictions of simplified SGHAT-type simulation modes, such as those shown in **Figure 12**, with possible real-world reflectivity behaviour of operational panel modes as shown in **Figure 13**.

## 6 GLARE IMPACT ASSESSMENT - RESULTS

### 6.1 Aviation Sector Reflective Glare

Narromine Aerodrome (ICAO: YNRM) is located to the north of the Project site, with the northern perimeter of the site approximately 1 km from the southern thresholds of its two runways. The aerodrome is serviced by general aviation aircraft and helicopters.

- The aerodrome's 1,521 m asphalt/grass Runway 11/29 is oriented roughly northwest-southeast.
- The aerodrome's 1,100 m asphalt/grass Runway 04/22 is oriented roughly northeast-southwest.
- The aerodrome's glider-only, 848 m grass Runway 18/36 is oriented roughly north-south.
- The aerodrome does not have a control tower (and as far as is known to SLR, none is planned).

**Figure 3** shows (landing) flight paths of interest:

- Aircraft using Runway 04 and Runway 29 (approaching from the southwest and southeast respectively) would have a line of sight towards the Project and potential associated reflections on final approach and up until the last kilometre when the facility would be "behind" the line of site of pilots.
- Although aircraft using Runway 22 and Runway 11 (approaching from the northeast and northwest respectively) would have a line of sight towards the Project, the risk of glare will be negligible (in fact zero) given the maximum possible angles of reflected rays (early morning and late afternoon) – refer **Table 3** and **Figure 10**.
- Gliders using Runway 36 (approaching from the south) would have a line of sight towards the Project and potential associated reflections on final approach and up until the last mile (1.6 km) when the facility would be "behind" the line of site of pilots.
- Helicopter flight paths can be highly variable and landing approach paths in the direct line of sight of the Project are possible, although there is greater flexibility in adjusting helicopter flight paths if required.

Accordingly, a quantitative analysis was carried out using the Sandia Labs Solar Glare Hazard Analysis Tool (SGHAT) software tool to examine potential worst-case scenario flight path approaches and take-offs and their ability to create adverse and unacceptable glare (and glint) conditions.

- The aircraft flight paths are all for landing scenarios (worst-case with the pilot looking downwards).

The flights paths assessed for the Project are shown in **Figure 3**.

#### SGHAT Modelling Assumptions:

- All runway approaches shown in **Figure 3** were examined.
- Landing flight paths are aligned with their respective runways.
- All aircraft landing flight paths are 2 miles in length, on a 3° glide angle (standard SGHAT protocol).
- The SGHAT analysis examines ALL possible solar angles throughout the year – in 1-minute intervals.
- The reflectivity of the PV panels was assumed to be the same as that shown in the standard solar glass shown in **Figure 11**.

In terms of the relative heights of flight paths and the solar farm:

- Ground elevations (ASL) of Narromine West Solar Farm range from 236 m to 240 m;
- Ground elevations below the various flight paths are in the range 234 m to 240 m.

From the above, it can be seen that the terrain in the Narromine area is reasonably flat, with all surrounding receivers (residences, vehicles) at similar elevations compared to the solar farm.

A number of panel scenarios were assessed:

- “Normal Tracking”: panels tilt  $\pm 60^\circ$  about a north-south horizontal axis  
– this would be the normal operational mode for the solar farm;
- “Fixed Tilt”: panels remain fixed at angles of  $0^\circ$  (horizontal) and  $\pm 15^\circ$   
– this is a scenario theoretically possible under a situation involving: shutdown, maintenance, pre-commissioning, etc
- “Tracking + Stowed”: panels tilt  $\pm 60^\circ$  about a north-south horizontal axis  
and then rest for the remainder of the time at a fixed angle of  $0^\circ$

#### SGHAT Results – “NORMAL TRACKING $\pm 60^\circ$ ”

The SGHAT Ocular Plots results for this scenario for all flight paths shown in **Figure 3** excluding gliders are presented in **Table 4**, which shows the total number of minutes in a year that solar panel reflections would be potentially visible within any relevant SGHAT “zone” (refer **Figure 7**).

It will be recalled that solar panel reflections (glint and glare) are acceptable according to the FAA-SGHAT protocol if there are no “Yellow” zone or “Red” zone results for aircraft flight landing paths.

For all runways, the SGHAT analysis yields “zero” glare conditions.

**Table 4 SGHAT Analysis Results ( No of Minutes Reflections are in SGHAT Zones )**

Flight Landing Path ( refer Fig.3 )	SGHAT Results for “NORMAL TRACKING” $\pm 60^\circ$ Scenario		
	“Green” Zone	“Yellow” Zone	“Red” Zone
Runway 11	0	0	0
Runway 29	0	0	0
Runway 04	0	0	0
Runway 22	0	0	0

#### SGHAT Results – FIXED TILT Scenarios ( $30^\circ$ , $15^\circ$ , $7.5^\circ$ West, $0^\circ$ and $7.5^\circ$ , $15^\circ$ , $30^\circ$ East )

The SGHAT Ocular Plots results for these scenarios for all flight paths shown in **Figure 3** excluding gliders are presented in **Table 5**, which shows the total number of minutes in a year that solar panel reflections would be potentially visible within any relevant SGHAT “zone” (refer **Figure 7**).

It will be recalled that solar panel reflections (glint and glare) are acceptable according to the FAA-SGHAT protocol if there are no “Yellow” zone or “Red” zone results for aircraft flight paths.

**Table 5 SGHAT Analysis Results ( No of Minutes Reflections are in SGHAT Zones )**

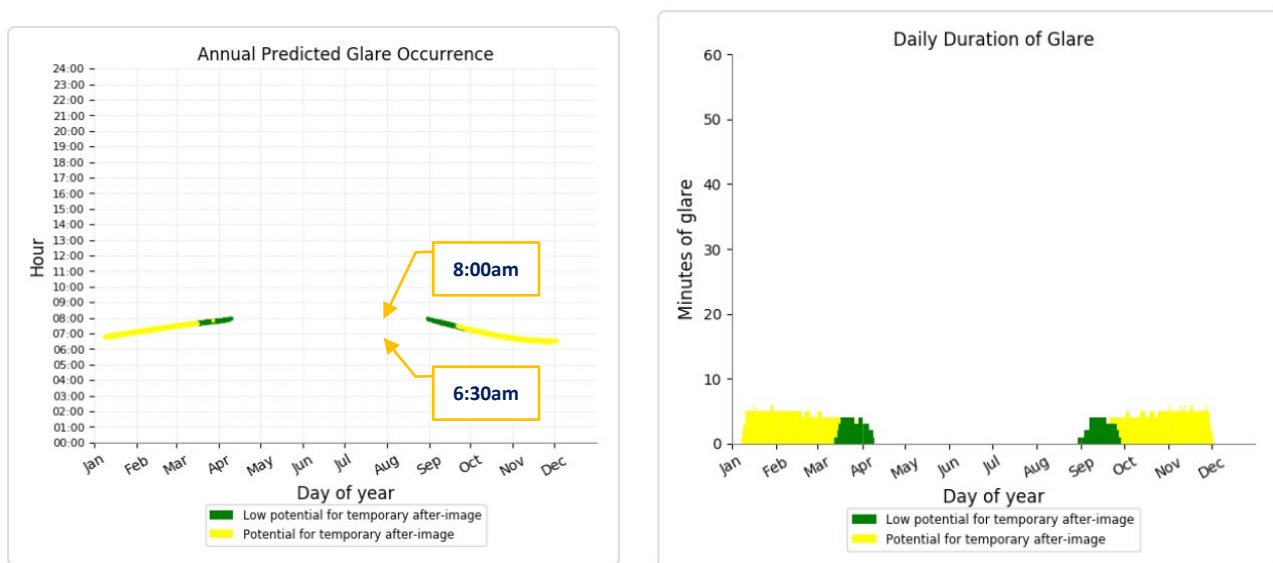
Flight Landing Path ( Fig.3 )	SGHAT Results for "FIXED TILT" Scenarios													
	30° West		15° West		7.5° West		0° ( Horizontal )		7.5° East		15° East		30° East	
	Green Zone	Yellow Zone	Green Zone	Yellow Zone	Green Zone	Yellow Zone	Green Zone	Yellow Zone	Green Zone	Yellow Zone	Green Zone	Yellow Zone	Green Zone	Yellow Zone
Runway 11	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Runway 29	0	0	0	0	0	0	438	0	227	<b>424</b>	451	0	195	0
Runway 04	493	0	802	<b>9</b>	173	<b>629</b>	221	<b>443</b>	0	0	0	0	0	0
Runway 22	0	0	0	0	0	0	0	0	0	0	0	0	0	0

### Representative Results – 7.5° FIXED Tilt WEST / Runway 04

**Figure 14** shows representative reflection conditions occurring at different times of the year for Narromine Aerodrome Runway 04:

- Reflections are visible between early January to early April and the start of September to end of November in the early morning (low altitude solar rays); during this period, reflections are visible for periods ranging up to 5 minutes each day.

**Figure 14 Selected SGHAT Results: FIXED TILT 7.5° WEST Mode (Runway 04)**

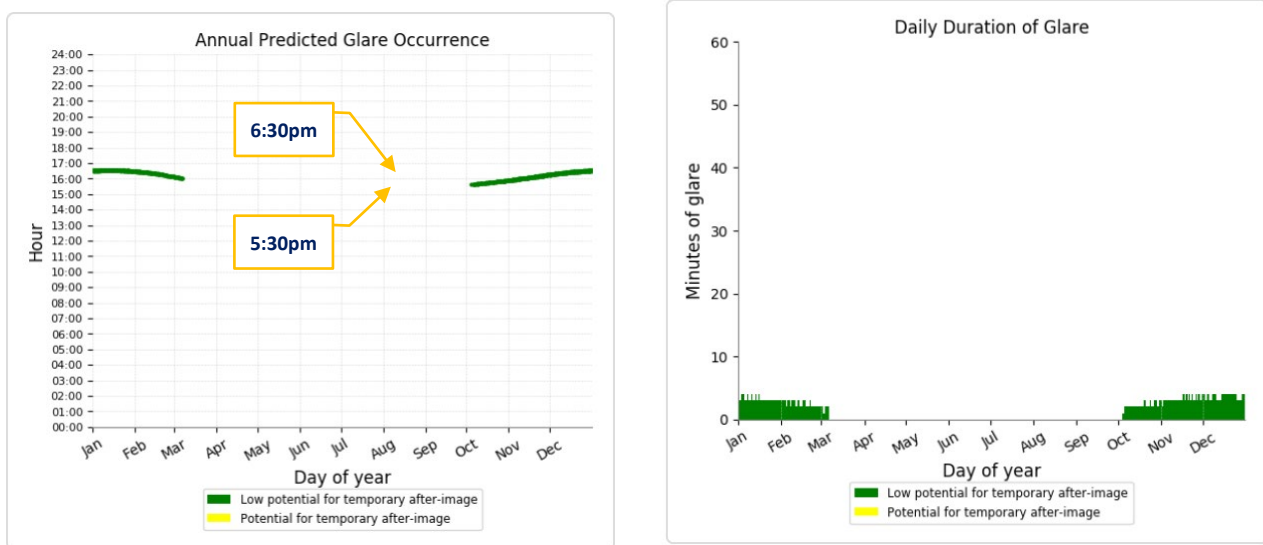


### Representative Results – 15° FIXED Tilt EAST / Runway 29

**Figure 15** shows representative reflection conditions occurring at different times of the year for Private Airstrip Runway 06:

- Reflections are visible from the start of October through to the start of March (relatively low altitude solar rays during summer months) in the late afternoon; during this period, reflections are visible for only very periods typically around 2-3 minutes each day.

**Figure 15 Selected SGHAT Results: FIXED TILT 15° WEST Mode (Runway 29)**



### SGHAT Results – TRACKING + FIXED TILT 0° Scenario

The SGHAT Ocular Plot results for this scenario for all flight paths shown in **Figure 3** are presented in **Table 6**, which shows the total number of minutes in a year that solar panel reflections would be potentially visible within any relevant SGHAT “zone” (refer **Figure 7**).

It will be recalled that solar panel reflections (glint and glare) are acceptable according to the FAA-SGHAT protocol if there are no “Yellow” zone or “Red” zone results for aircraft flight paths.

**Table 6 SGHAT Analysis Results ( No of Minutes Reflections are in SGHAT Zones )**

Flight Landing Path ( ref Fig.3 )	SGHAT Results for “±60° TRACKING + 0° FIXED TILT” Scenario		
	“Green” Zone	“Yellow” Zone	“Red” Zone
Runway 11	0	0	0
Runway 29	438	0	0
Runway 04	221	<b>443</b>	0
Runway 22	0	0	0

### Representative Results

The representative reflection conditions occur at exactly the same times of the year and for the same durations as shown in **Table 4**. In both cases, the solar panels are horizontal at sunrise enabling the visibility of reflections essentially from the same direction as the incoming (direct) solar rays.



## SGHAT Results – GLIDER Operations Runway 18/36

The SGHAT Ocular Plot results for this scenario for the glider flight paths shown in **Figure 3** are presented in **Table 7**, which shows the total number of minutes in a year that solar panel reflections would be potentially visible within any relevant SGHAT “zone” (refer **Figure 7**).

It will be recalled that solar panel reflections (glint and glare) are acceptable according to the FAA-SGHAT protocol if there are no “Yellow” zone or “Red” zone results for aircraft flight paths.

**Table 7 SGHAT Analysis Results ( No of Minutes Reflections are in SGHAT Zones )**

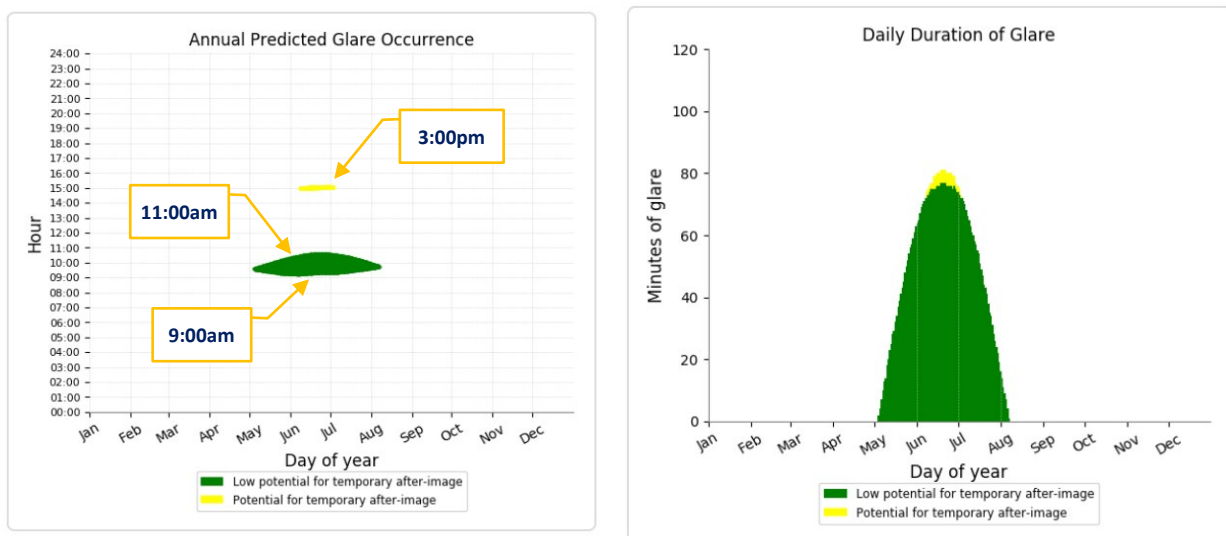
Flight Landing Path ( ref Fig.3 )	SGHAT Results for “±60° TRACKING + 0° FIXED TILT” Scenario		
	“Green” Zone	“Yellow” Zone	“Red” Zone
Runway 18	0	0	0
Runway 36	4811	82	0

## Representative Results

**Figure 16** shows representative reflection conditions occurring at different times of the year for Narromine Aerodrome Runway 36, assuming a 3° glide path on landing:

- Reflections are visible for around 3 months around mid-winter, with the vast majority of occurrences occurring mid-morning and in the SGHAT “green” zone;
- For approximately a month around the winter solstice, reflections in the SGHAT “yellow” zone occur at around 3:00 pm, averaging 3 minutes per day. This occurs when the array panels are brought back to a horizontal position at the end of their daily period normal tracking.

**Figure 16 Selected SGHAT Results: FIXED TILT 15° WEST Mode (Runway 29)**



## Summary of SGHAT Results:

The various reflection conditions are summarised in **Table 8** for the “±60° Normal Tracking” mode scenarios and the “Fixed Tilt” modes: 30°, 15°, 7.5° West, 0° (horizontal) and 7.5°, 15°, 30° East. The combined “±60° Tracking + FIXED TILT 0°” mode results are not shown as they are identical to the “Fixed Tilt” 0° (horizontal) results.

Solar panel reflections (glint and glare) are acceptable according to the FAA-SGHAT protocol if there are no “Yellow” zone or “Red” zone results for aircraft flight paths.

**Table 8 SGHAT Analysis Summary Results - SGHAT Compliance**

Panel Mode Scenario	Runway 04	Runway 29	Runways 11, 22, 18	Runway 36 (GLIDERS only)
“±60° Normal Tracking”	Complies	Complies	Complies	Complies
“Fixed Tilt” mode: 30° West	Complies	Complies		
“Fixed Tilt” mode: 15° West	Complies	Complies		
“Fixed Tilt” mode: 7.5° West	Does Not Comply	Complies		
“Fixed Tilt” mode: 0° (horizontal)	Does Not Comply	Complies		Does Not Comply
“Fixed Tilt” mode: 7.5° East	Complies	Does Not Comply		
“Fixed Tilt” mode: 15° East	Complies	Complies		
“Fixed Tilt” mode: 30° East	Complies	Complies		

## Recommendations:

### Normal Tracking Mode:

- The proposed solar farm will comply with SGHAT requirements under standard “±60° Normal Tracking” mode, where the panels are at 60° eastwards from sunrise until the solar altitude angle reaches 30° above the horizon, at which time that commence tracking the sun until the solar angle reaches 30° above the horizon(to the west), where they then remain until sunset.

### Non-Normal Operational Modes:

There may be situations where solar panels need to be left at or near horizontal tilt angles, eg for maintenance purposes, during construction, etc, or in “back-tracking” mode at the start and end of the day. In this instance:

- Solar panels could be left with either an eastwards or westwards tilt of a minimum 15° during the months when “YELLOW” SGHAT glare is predicted to occur – refer **Figures 14 and 16**.
- Note that this would also eliminate the potential for glare for gliders using Runway 36.

## 6.2 Motorist “Disability” Glare and Pedestrian ‘Discomfort’ Glare

The “major” and “minor” thoroughfares in the immediate vicinity of the Project are shown in **Figure 4**, including:

- |  |         |
|--|---------|
| • Mitchell Highway – eastbound and westbound     | “major” |
| • Dandaloo Road - eastbound and northbound       | “minor” |
| • Old Blackwater Road - eastbound and northbound | “minor” |
| • McNamaras Lane – northeast bound               | “minor” |
| • Second Avenue – westbound                      | “minor” |

The relevant TI criteria for the above roads would be:

- For (Motorist) Traffic Disability Glare, the TI Value should remain below 20 for “minor” roads and below 10 for “major” roads; and
- For Pedestrian Discomfort Glare, the TI Value should remain below 2 at pedestrian crossings and below 3 for other locations.

Important factors influencing the potential for traffic disability glare include:

- Any difference in elevation between the motorist and the solar panel array;
- The potential for solar reflections of concern to be obstructed by intervening terrain and topography as well as dense vegetation;
- The difference between the line of sight of a driver (i.e. in the direction of the road) and the line of sight relative to incoming reflections. Significant TI values can only occur when this difference is small. In some cases, eg when traffic is moving away from the line of incoming reflections, such reflections become essentially invisible to the motorist – this would apply for example to traffic on Dandaloo Road travelling eastwards after passing the site.

**Figure 17** shows that some of the potential road glare scenarios for the Project site. The difference between the line of sight of a driver and the Project (and hence potential reflections) varies from modest, as in the case of Dandaloo Road, to reasonable (ie not small) as in the case of the Mitchell Highway.

**Figure 17 View of the Project from Surrounding Roads**

Driving east along  
Dandaloo Road



( Fig.17 cont'd )

Driving west along  
Mitchell Highway



SLR has undertaken TI Value calculations for the roadways discussed above. Calculation locations were varied along the relevant carriageways, focussing on positions where the line of sight of drivers was close to the angle of potential incoming solar reflected rays.

**Table 9** shows the results for the standard “ $\pm 60^\circ$  Normal Tracking” mode.

**Table 10** shows combined results for the various FIXED TILT scenarios.

**Table 9 TI Value Results – Results for NORMAL TRACKING**

Carriageway ( class )		TI Value	Occurrence	
			Time of Year / Hour	Duration/Day
Mitchell Highway ( major )	eastbound	nil	all-year-round	na
	westbound	nil	all-year round	na
Dandaloo Road ( minor )	eastbound	nil	all-year-round	na
	westbound	nil	all-year round	na
Old Blackwater Road ( minor )	eastbound	nil	all-year-round	na
	westbound	nil	all-year round	na
McNamaras Lane ( minor )	northeast	nil	all-year-round	na
Second Avenue ( minor )	westbound	nil	all-year-round	na

**Table 10 TI Value Results – Combined Results for ALL FIXED TILT Scenarios**

Carriageway ( class )		TI Value	Occurrence	
			Time of Year / Hour	Duration/Day
Mitchell Highway ( major )	eastbound westbound	nil Max 10	all-year-round 4 months: mid-summer / late afternoon	na 2 min/day
Dandaloo Road ( minor )	eastbound westbound	Max 12 Max 8	2 months (Apr,Aug) / early morning 2 months (Apr,Aug) / late afternoon	10 min / day 2 min / day
Old Blackwater Road ( minor )	eastbound westbound	Max 4 nil	5 months (winter) / early morning all-year round	3 min / day na
McNamaras Lane ( minor )	northeast	nil	all-year-round	na
Second Avenue ( minor )	westbound	Max 2	2 months (equinoxes) / late afternoon	2 min / day

The TI calculation results shown in **Table 9** for “normal” tracking mode indicate the following:

- TI Values registered for ALL carriageways will be zero at all times of the year.

The reasons for this result are:

- Essentially the same elevation for motorists and the solar array panels; and
- The single axis trackers which support the panels – these cause outgoing reflections for all incoming solar angles to be redirected upwards away from the ground.

The TI calculation results shown in **Table 10** for “zero tilt” modes indicate the following:

- Reflections will be visible from a number of surrounding carriageways (depending on tilt angle); and
- TI Values registered for all carriageways are below their acceptable limiting values.

In the above computations, no advantage was taken of the vegetation present in the area. Examples of this vegetation are shown in **Figure 18**.



**Figure 18 Vegetation Examples Surrounding the Project Site**



### 6.3 Rail Operator Reflective Glare

**Figure 5** shows the Main Western Railway Line approaching Narromine from the east and then moving towards the northwest and the Parkes-Narromine Railway Line approaching Narromine from the south prior to turning eastwards and joining up with the Main Western Railway Line. At their closes approach points, the Main Western and Parkes-Narromine Railway Lines are 350 m and 800 m from the nearest Project site location respectively.

SLR has undertaken TI Value calculations for sections of rail lines as shown in **Figure 19**, focussing on positions where the line of sight of train drivers was closest to the angle of potential incoming solar reflected rays.

- For the standard operational “ $\pm 60^\circ$  Normal Tracking” mode, the TI Values for Disability Glare were NIL.
- For the FIXED TILT eastwards scenarios, reflections are visible on the Main Western Railway Line for periods ranging up to 2-3 minutes per day from mid-August through to mid-April, ranging from 5:00 pm to 6:00 pm depending on the time of year. The associated TI Values are modest and well below the limiting criteria of  $TI=20$ .

**Figure 19 Walgett Railway Line – Glare Assessment Areas**



## 6.4 Industrial Critical Machinery Operators

There are no industrial operations in the vicinity of the Project (e.g. mining operations) and none planned (mining or otherwise), with the kind of machinery where the relevant operators have the potential to experience reflective glare from the Project, eg elevated cabins in draglines, etc.

## 6.5 Residential “Nuisance” Glare

The nearest residential receivers to the Project are identified in **Figure 6**.

- They surround the site at varying distances from the nearest respective site boundary.
- Their ground elevations are similar to the Project, with only selected receivers minimally higher.

There are no formal TI Value (or alternative) criteria governing reflective glare from solar facilities.

Accordingly, SLR has carried out TI Value calculations for the receivers discussed above, to gain an understanding of the potential for nuisance glare conditions from the project. The results are shown in **Table 11**.

Note again that, in the residential receiver computations, no advantage was taken of the vegetation present in the area – refer examples shown in **Figure 18**.

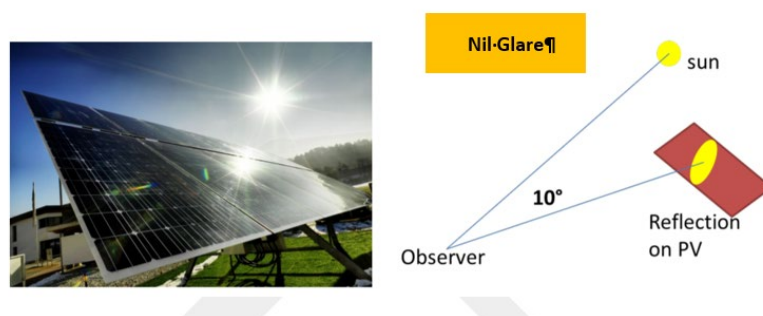
**Table 11 TI Value Results – Residential Receivers**

Scenario	Receivers (refer Figure 6)	TI Value	Occurrence	
			Time of Year / Hour	Duration/Day
±60° Normal Tracking	R1 to R15	nil	all-year-round	na
Fixed Tilt 15° EAST, 0°	R1-R3, R5-R8 R4	Up to TI ~ 3	2 months / late afternoon	0-3 min /day
		up to TI ~ 6	8 months / late afternoon	0-18 min /day
Fixed Tilt 15° WEST	R11 to R15	Up to TI ~ 3	6 months / early morning	0-6 min /day

The results indicate the following:

- For the standard operational “±60° Normal Tracking” mode, the TI Values were NIL at all receivers;
- For the FIXED TILT eastwards and FIXED TILT 0° scenarios, reflections will be potentially visible for a number of receivers to the east of the site, in particular Receiver 4, for periods ranging up to 8 months of the year and up to 18 minutes per day (for Receiver 4). The associated TI Values are potentially highest at Receiver 4. Note that for all other receivers, the blockage provided by vegetation, trees, etc, will effectively eliminate any remaining glare issues (refer **Figure 18**).
- For the FIXED TILT westwards scenarios, reflections will also be potentially visible for a number of receivers to the west of the site, in particular Receiver 13, for periods ranging up to 6 months of the year and up to 8 minutes per day during the winter months of April to August (for Receiver 13). However, when taking into account the blockage provided by vegetation, trees, etc (refer **Figure 18**), these reflection conditions should be effectively eliminated.
- Because these reflections all occur either early in the morning or late in the afternoon, visible reflections would be in the same line of sight as the solar rays themselves – this would not constitute a glare condition – as is shown in **Figure 20**, although as previously noted there are no actual criteria governing the acceptability or otherwise of such glare conditions.

**Figure 20 Nil Glare Condition for Residential Nuisance Glare**



If it is intended to avoid all potential residential glare issues (eg if the mere visibility of reflections was to cause an issue within the surrounding community) the following options are recommended to avoid all potential glare conditions IF it is expected that there will be instances when solar panels will be left in a horizontal or near horizontal position (eg for maintenance, during construction, etc).



- Provide a row of planting along the EAST perimeters of the facility such that the top of the vegetation is a minimum 1 m above the height of the solar panel axis height, which varies up to approximately 1.8 m above local ground level – refer **Figure 21**;

OR

- Avoid fixed tilt scenarios for the facility during the months when reflections would be visible at Receiver 4 – ie late afternoon for the winter half of the year (March to September).

**Figure 21 Proposed Project Site Perimeter Landscaping**



## 6.6 Night-Time Illumination Glare

Although presently not fully defined, it is assumed that an area within the Narromine West Solar Farm Project site will be set aside for an Operation and Maintenance buildings, power conversion unit, fire access routes and egress, etc, and that some of these may need to be operational 24/7.

Although night-time illumination is not presently planned for the Project, it may be required in the future for some of the above relevant areas and, as such, is addressed in principle in this assessment.

The only potential for any future night-time illumination glare would be associated with the nearest thoroughfares and residential and other sensitive receivers to the Project. Consideration has also been given to the potential for adverse eco-lighting impacts on nocturnal fauna habitats in close proximity to the Project site, especially within any close-by native vegetation areas. On the basis of the Flora and Fauna Assessment Report carried out for the Project, there are no such habitats close to the Project site.

The recommendations set out below are therefore made in the event that future 24/7 lighting is incorporated into the Project, to achieve the best lighting performance (taking into account safety considerations) while having a minimal impact on the surrounding properties, carriageways and nocturnal fauna.

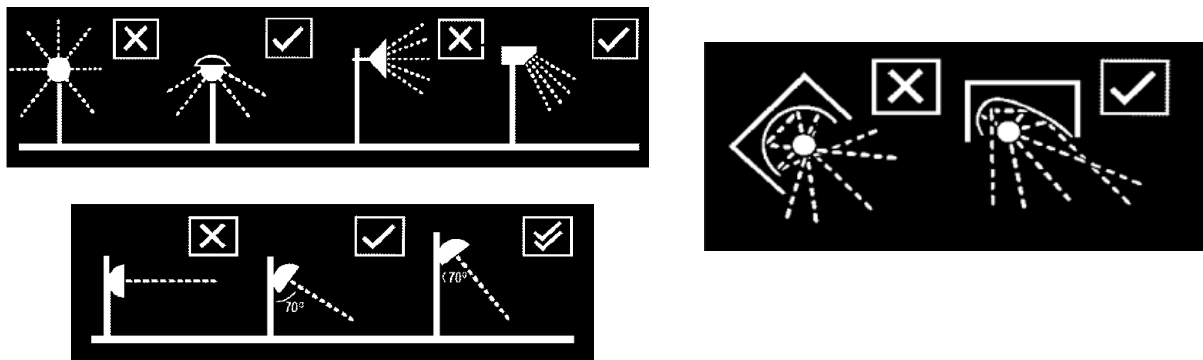
In terms of any future potential night-time lighting, the adopted goal of limiting night-time light spill to no more than 1 lux falling on the nearby residential facades during curfew hours will be easily achieved given the distances to the nearest residential and other receivers.

Accordingly, the potential for any future nuisance glare will be non-existent.

AS4282-1997 *Control of the Obtrusive Effect of Outdoor Lighting* sets out general principles that should be applied when designing outdoor light to minimise any adverse effect of the light installation.

- Direct lights downward as much as possible and use luminaires that are designed to minimise light spill, e.g. full cut-off luminaires where no light is emitted above the horizontal plane, ideally keeping the main beam angle less than 70°. Less spill-light means that more of the light output can be used to illuminate the area and a lower power output can be used, with corresponding energy consumption benefits, but without reducing the illuminance of the area - refer **Figure 22**.
- Do not waste energy and increase light pollution by over-lighting.
- Wherever possible use floodlights with asymmetric beams that permit the front glazing to be kept at or near parallel to the surface being lit.

**Figure 22 Luminaire Design Features that Minimise Light Spill**



## 7 CONCLUSION

SLR Consulting Australia Pty Ltd (SLR) has been engaged to carry out a Reflective Glare assessment of the proposed Narromine West Solar Farm (the “Project”) under development by Providence Asset Group. The proposed (up to) 5 MWac facility will comprise 12,348 solar PV panels within a 15 ha project site area. The 540 W panels, measuring approximately 2.26 m by 1.13 m, will be positioned as currently understood on single-axis trackers oriented north-south with a spacing of 6.25 m. The Project is located close to the township of Narromine and Narromine Aerodrome.

The following potential glare conditions have been considered:

- Daytime Reflective glare (and glint) arising from the solar PV panels within the facility:
  - . Aviation Sector Reflective Glare;
  - . Motorist “Disability” Reflective Glare and Pedestrian “Discomfort” Reflective Glare;
  - . Rail Operator Reflective Glare;
  - . Industrial critical machinery operators (heavy vehicles, etc) Reflective Glare; and
  - . Residential “Nuisance” Glare
- Night-time Illumination glare if any 24/7 operational security lighting is incorporate into the Project in the future. It is noted that lighting is NOT currently planned.

### Aviation-Related Potential Glare

Quantitative analysis using the FAA-SGHAT software tool has shown that there will be nil glare from the Project at Narromine Aerodrome with the solar array in normal tracking mode, ie panels tilting  $\pm 60^\circ$ .

There is potential for glare if panels need to be left at a near horizontal angle. Leaving the solar array with either an eastwards or westwards fixed tilt angle of at least  $15^\circ$  would eliminate this occurrence. This will also eliminate any potential for glider operational glare on Runway 36.

### Motorist, Rail Traffic and Residential Glare

There will be nil glare from the Project in relation to road traffic, rail traffic and surrounding residential receivers under the standard operational  $\pm 60^\circ$  tilt angle scenario.

There is potential for reflection visibility, although not reflective glare, to nearby residential receivers if solar panels are left in a FIXED TILT horizontal or near horizontal position (eg for maintenance, during construction, under back-tracking mode, etc), mainly applying to Receiver 4 east of the site. To eliminate the visibility of reflections entirely at Receiver 4, perimeter landscaping along the eastern perimeter of the site or avoiding fixed tilt angle east scenarios during late afternoon of winter months has been recommended.

### Night-Time Illumination Glare

Although presently not incorporated into the Project, consideration has been given to the future potential for night-time lighting related to equipment and/or buildings, fire access routes and egress, etc. Recommendations have been made to ensure that the potential for any future possible night-time illumination glare will be non-existent. Any future lighting design should also be checked against the requirements of CASA’s NASF Guidelines.

## ASIA PACIFIC OFFICES

### BRISBANE

Level 2, 15 Astor Terrace  
Spring Hill QLD 4000  
Australia  
T: +61 7 3858 4800  
F: +61 7 3858 4801

### MACKAY

21 River Street  
Mackay QLD 4740  
Australia  
T: +61 7 3181 3300

### ROCKHAMPTON

rockhampton@slrconsulting.com  
M: +61 407 810 417

### AUCKLAND

68 Beach Road  
Auckland 1010  
New Zealand  
T: +64 27 441 7849

### CANBERRA

GPO 410  
Canberra ACT 2600  
Australia  
T: +61 2 6287 0800  
F: +61 2 9427 8200

### MELBOURNE

Suite 2, 2 Domville Avenue  
Hawthorn VIC 3122  
Australia  
T: +61 3 9249 9400  
F: +61 3 9249 9499

### SYDNEY

2 Lincoln Street  
Lane Cove NSW 2066  
Australia  
T: +61 2 9427 8100  
F: +61 2 9427 8200

### NELSON

5 Duncan Street  
Port Nelson 7010  
New Zealand  
T: +64 274 898 628

### DARWIN

5 Foelsche Street  
Darwin NT 0800  
Australia  
T: +61 8 8998 0100  
F: +61 2 9427 8200

### NEWCASTLE

10 Kings Road  
New Lambton NSW 2305  
Australia  
T: +61 2 4037 3200  
F: +61 2 4037 3201

### TAMWORTH

PO Box 11034  
Toowoomba NSW 2340  
Australia  
M: +61 408 474 248  
F: +61 2 9427 8200

### NEW PLYMOUTH

Level 2, 10 Devon Street East  
New Plymouth 4310  
New Zealand  
T: +64 0800 757 695

### GOLD COAST

Ground Floor, 194 Varsity  
Parade  
Varsity Lakes QLD 4227  
Australia  
M: +61 438 763 516

### PERTH

Ground Floor, 503 Murray Street  
Perth WA 6000  
Australia  
T: +61 8 9422 5900  
F: +61 8 9422 5901

### TOWNSVILLE

Level 1, 514 Sturt Street  
Townsville QLD 4810  
Australia  
T: +61 7 4722 8000  
F: +61 7 4722 8001